

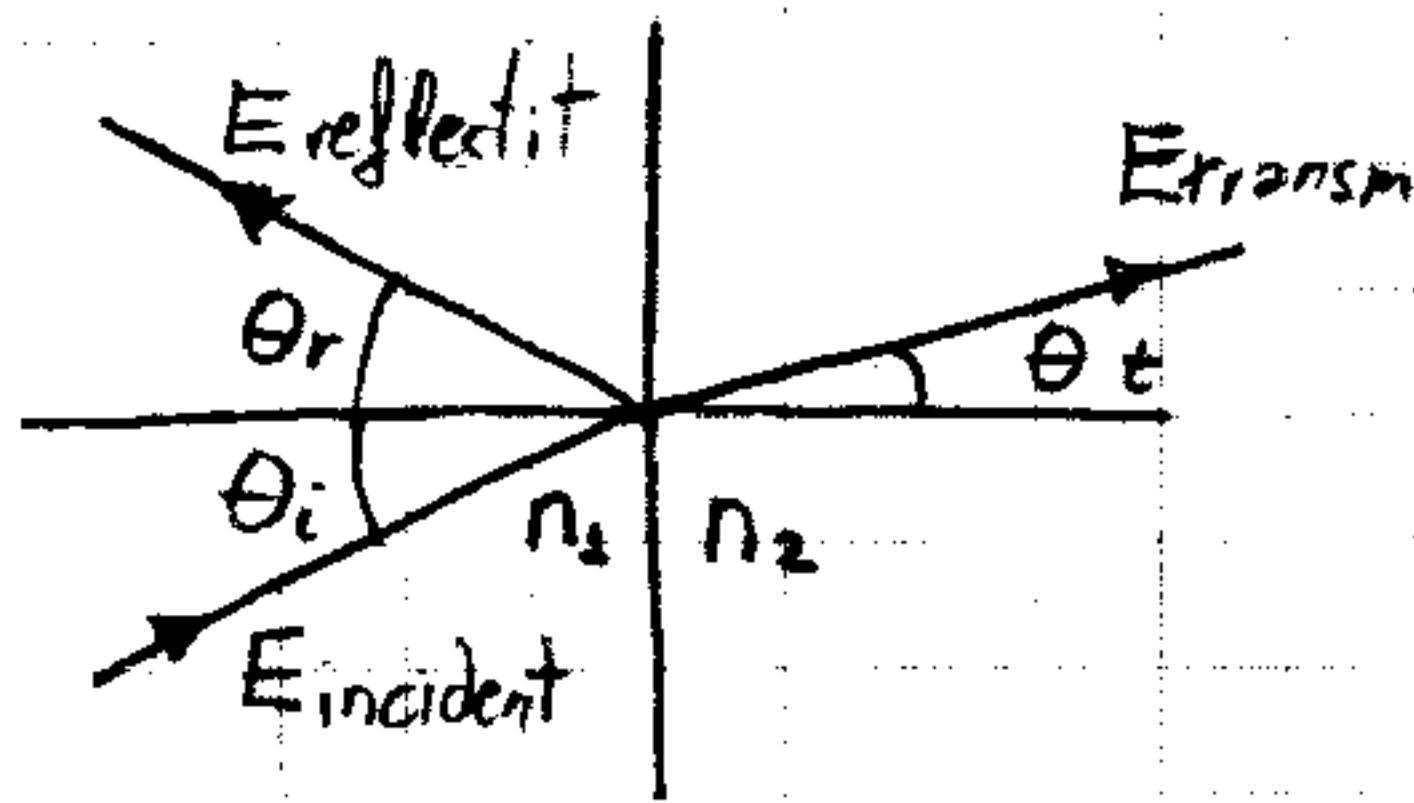
COMUNICACIONES ÓPTICAS

T-1 INTRODUCCIÓ

$$V_{prop} = c/n$$

Llei de reflexió

$$\theta_i = \theta_r$$



Llei de Snell

$$n_1 \sin \theta_i = n_2 \sin \theta_t$$

$$r = \frac{E_{reflex}}{E_{incid}}$$

$$R = |r|^2$$

Reflectivitat

- Reflexió total

$$\theta_i \geq \theta_c$$

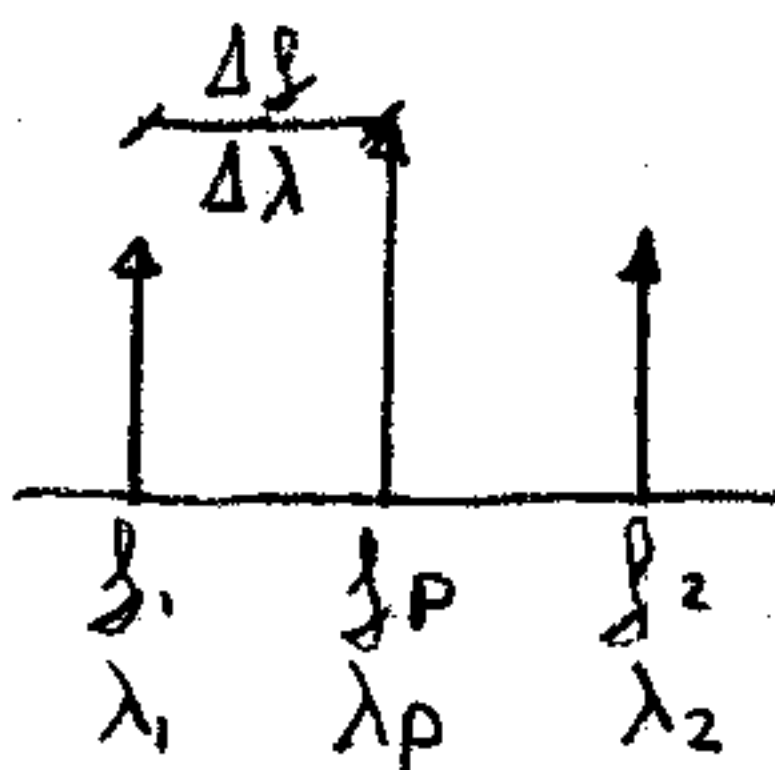
$$\theta_c = \arcsin \frac{n_2}{n_1}$$

($n_2 < n_1$)

- Índex de refracció relatiu

$$\Delta \triangleq \frac{n_1 - n_2}{n_1}$$

- Relació $\Delta\lambda - \Delta\beta$



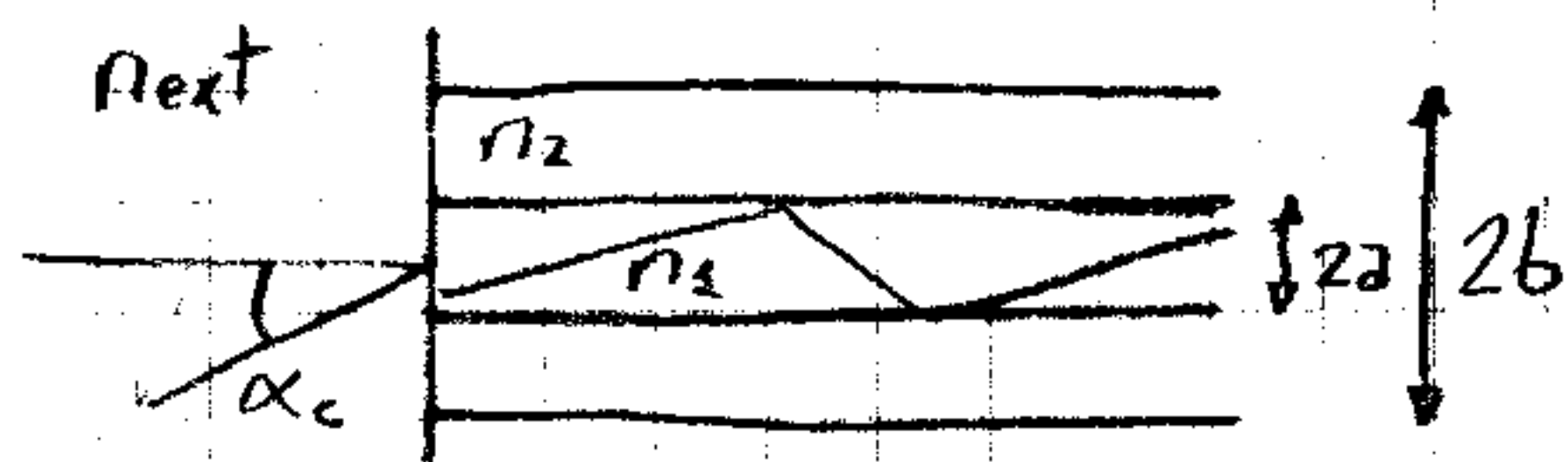
$$\frac{\Delta\lambda}{\lambda_p} \approx \frac{\Delta\beta}{\beta_p}$$

$$c = \lambda_p \beta_p$$

- Atenuació:

$$1 \text{ dB/m} \equiv 8.686 \text{ Nep/m}$$

T-2 FIBRES ÒPTIQUES



Obertura numèrica

$$NA \triangleq \sin \alpha_c = \frac{\sqrt{n_1^2 - n_2^2}}{n_{ext}}$$

α_c : angle d'acceptació

- Finestres òptiques

1 μ	$\lambda = 850 \text{ nm}$	$\rightarrow \alpha = 2.5 \text{ dB/km}$	Molt ample
2 μ	$\lambda = 1300 \text{ nm}$	$\rightarrow \alpha = 0.5 \text{ dB/km}$	Molt estret
3 μ	$\lambda = 1550 \text{ nm}$	$\rightarrow \alpha = 0.22 \text{ dB/km}$	1550-1560 nm

- Freqüència normalitzada

$$V = \frac{2\pi a}{\lambda} a(NA)$$

$V > 2.405$ F.O. Multimodo

$V < 2.405$ F.O. Monomodo

- Fibres multimode de salt d'índex

modes $N_t^{SI} = \sqrt{2}$

Dispersió intermodal $\tau_{INTER}^{SI} \approx \frac{n_1}{c} \Delta$ [nseg/km]

- Fibres multimode de gradient d'índex

modes $N_t^{GRIN} = \sqrt{4}$

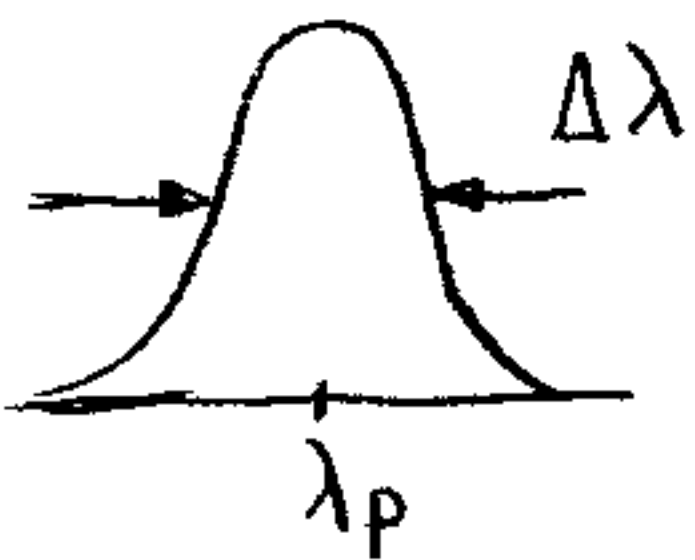
Dispersió intermodal

$\tau_{INTER}^{GRIN} \approx \frac{n_1}{c} \frac{\Delta^2}{8} \approx \frac{\Delta}{8} \tau_{INTER}^{SI}$

$B \propto 1/\tau_{INTER}$ [GHz·km]

$B^{GRIN} = \frac{8}{\Delta} B^{SI}$

- Fibres monomode



velocitat de grup $v_g = \frac{c}{n_g}$

$n_g \triangleq n - \lambda \frac{\delta n}{\delta \lambda}$

Dispersió del material

$D_M \triangleq \frac{\partial}{\partial \lambda} \left(\frac{1}{v_g} \right)$

Dispersió guia-ona

$D_w \approx - \frac{n_{g1} - n_{g2}}{c\lambda} \frac{1.984}{\sqrt{2}}$

$\tau_{INTRA} = \Delta\lambda |D_M + D_w|$

- Ample de Bda

$\sigma \cdot f_0 \approx 0.1874$

σ : Desviació tipus

f_0 : Ample de Bda per m

$\tau = 2\sigma$

- Ample de Bda elèctric vs Òptic

$B_{opt} = \sqrt{2} B_{elec}$

Màxima vel. transmissió

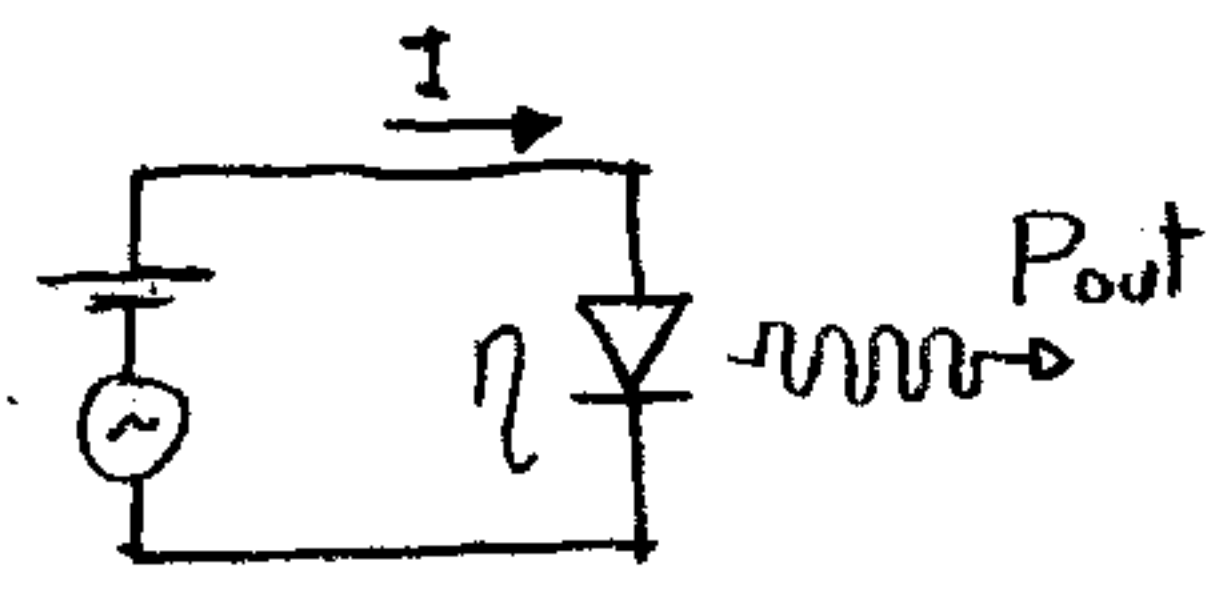
$R_B \leq 2 B_{elec}$

- Ample de Bda pràctic

$B_{opt}(L) = \frac{B_{opt}(1km)}{L^B}$

(multimode) $0.5 \leq \beta \leq 1$ (monomode)

1-3 FONTS ÒPTIQUES



$$P_{out} = \eta \cdot h\nu \frac{I}{q_e}$$

η : eficiència conversió elèctric-òptica

$$\langle n \rangle = \frac{P_{out}}{h\nu}$$

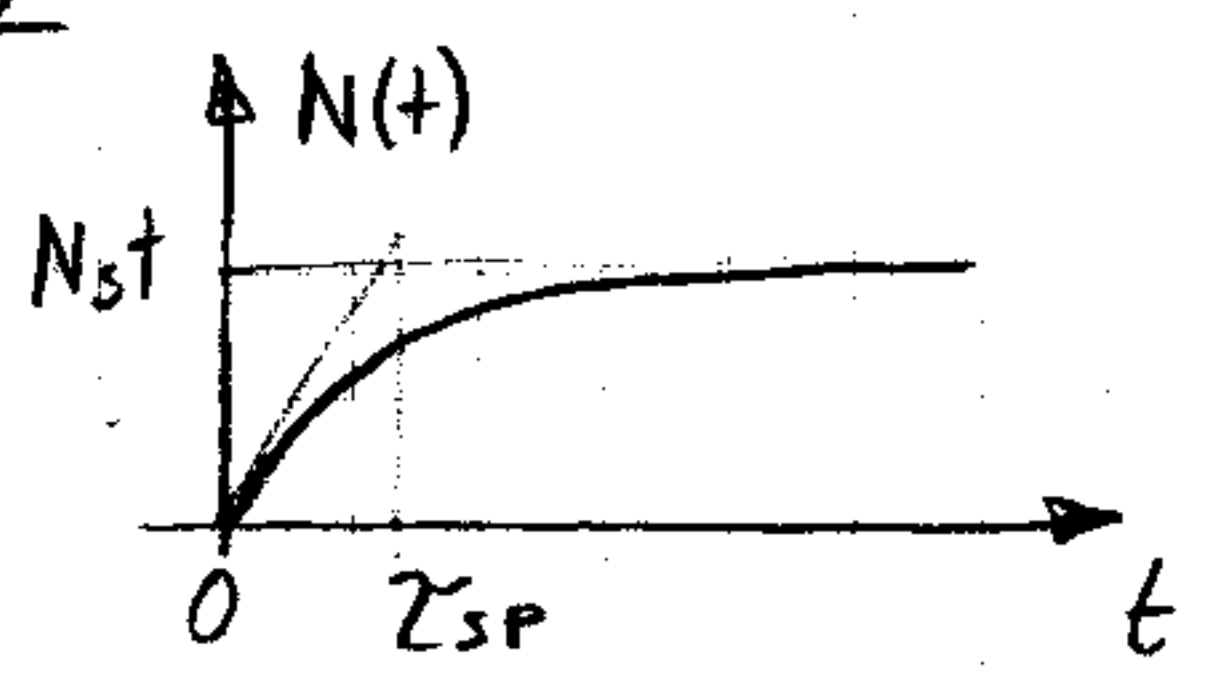
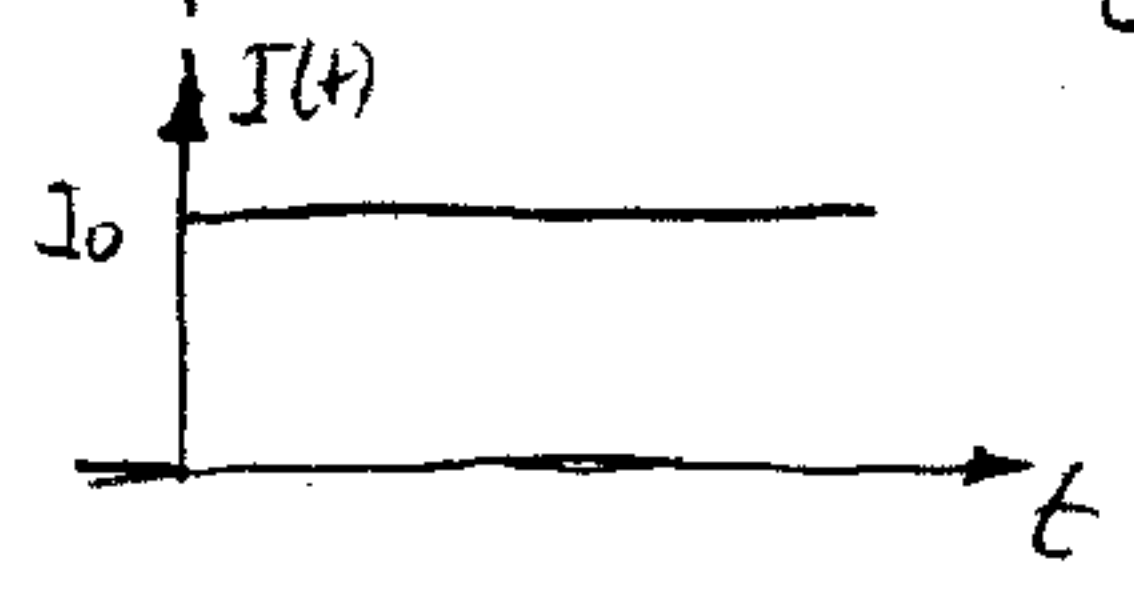
- DIODE LED

Ecuació de ritme

$$\frac{\partial N}{\partial t} = \frac{I}{qV} - \frac{N}{\tau_{sp}}$$

N : Densitat de portadors en z.A.
 τ_{sp} : Temps d'emissió espontànea

Resposta a l'esglaió



$$P_{out}(t) = \eta \frac{h\nu}{q} I_0 (1 - e^{-t/\tau_{sp}}) \quad | t_r = 2.197 \tau_{sp} |$$

$$T_B \approx 3 \tau_{sp} \text{ (conveni)} \Rightarrow R_B \leq 1/3 \tau_{sp}$$

Modulació sinusoidal

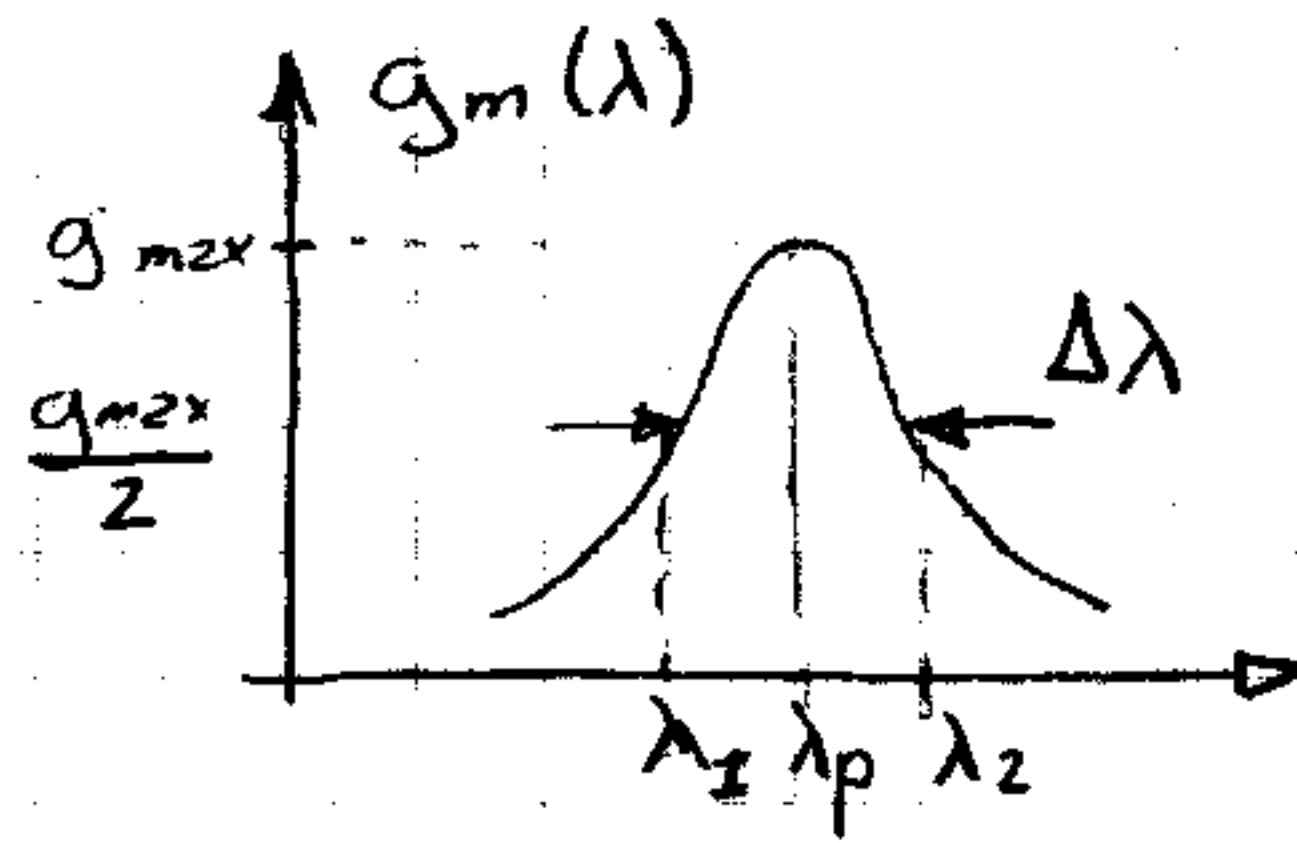
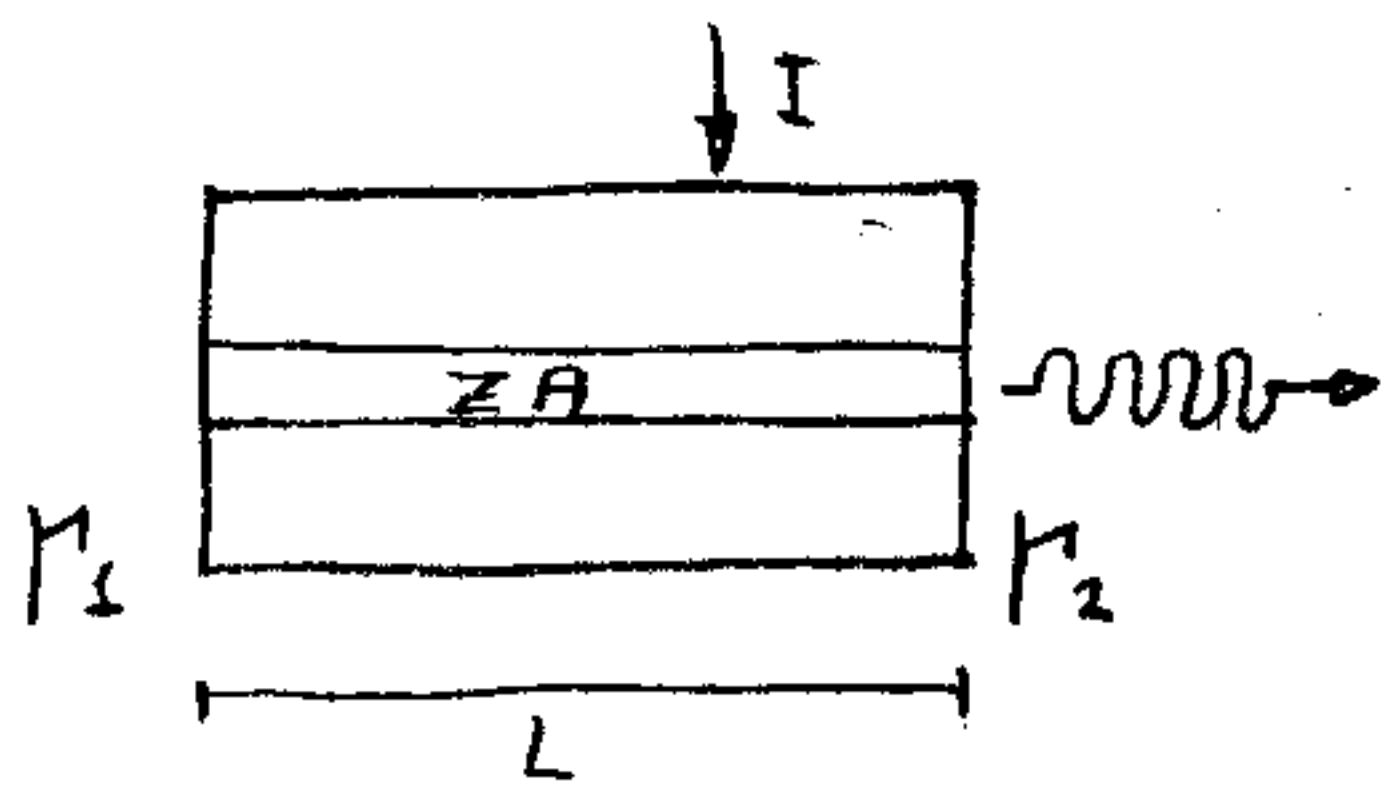
$$H(\omega) = \frac{R}{1 + j\omega \tau_{sp}} \quad R \triangleq \eta \frac{h\nu}{q}$$

$$B_{3dB} = \frac{1}{2\pi \tau_{sp}}$$

Perdues per acoblament LED-fibra

$$\frac{P_{injecc}}{P_{total}} = (NA)^2$$

- DIODE LASER



Guany

$$g_m \triangleq a(N - N_0)$$

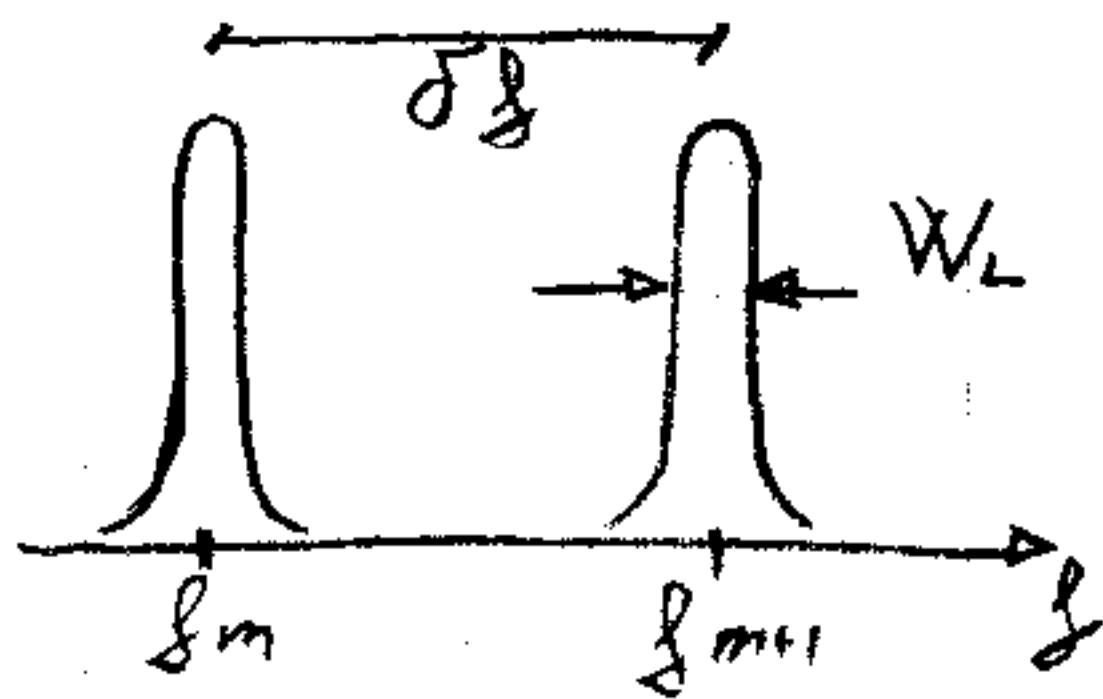
- Condició d'oscil·lació

$$g_n \geq g_{th} = \alpha_s + \frac{1}{2L} \ln \frac{1}{R_1 R_2} = \alpha_t$$

$$g_m = m \frac{v}{2L} \quad m \in \mathbb{Z}$$

α_s : perdes scattering

α_t : perdes totals



$$\zeta_{ph} \triangleq \frac{1}{v \alpha_t}$$

$$W_L \approx \frac{1}{2\pi \zeta_{ph}}$$

- Guany net de la llum en el medi

$$g(\lambda) = \Gamma g_m(\lambda)$$

Γ : factor de confinament

$$g_m(\lambda) = a(N - N_0) - \gamma(\lambda - \lambda_p)^2$$

- Condició d'arrencada del LASER

$$N > N_{th} \triangleq N_0 + \frac{\alpha_t}{a \Gamma}$$

$$I_{th} = \frac{qV}{\zeta_{ph}} N_{th}$$

Densidad de fotones

$$S = (N - N_{th}) \frac{\zeta_{ph}}{\zeta_{sp}} = (I - I_{th}) \frac{\zeta_{ph}}{qV}$$

$$R = \frac{I}{qV} = \frac{N}{\zeta_{sp}}$$

Si $R_1 = R_2 = R \Rightarrow$

$$S_{out} = \frac{1}{2} \frac{1-R}{\sqrt{R}} S_0$$

$$P_{out} = v h \nu W d S_{out}$$

$$S_0 \approx S$$

$$V = WLd \text{ (Volum)}$$

$$P_{out} = \frac{1-R}{2\sqrt{R}} \frac{h \nu}{q \alpha_t L} (I - I_{th})$$

- Modulació digital del LASER

◦ Cas 1 : $I_{OFF} < I_{th} < I_{ON}$

$$t_D = \tau \ln \frac{I_{ON} - I_{OFF}}{I_{ON} - I_{th}}$$

◦ Cas 2 : $I_{th} < I_{OFF} < I_{ON}$

$$t_{ON} = \left[\frac{2qV}{v\Gamma_a} \ln \left(\frac{I_{ON} - I_{th}}{I_{OFF} - I_{th}} \right) \frac{1}{I_{ON} - I_{OFF}} \right]^{1/2}$$

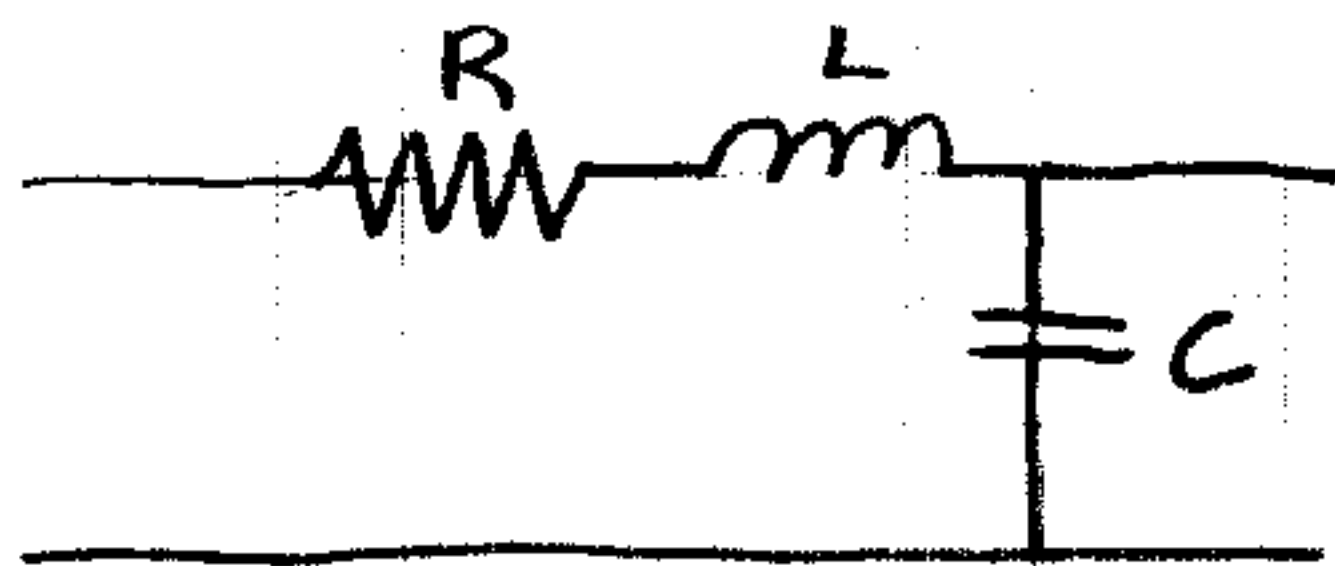
$$\frac{P_{ON}}{P_{OFF}} = \frac{I_{ON} - I_{th}}{I_{OFF} - I_{th}}$$

- Modulació analògica del LASER

$$I(t) = I_0 (1 + m \sin \omega_m t)$$

Relaxación : $\omega_r^2 \triangleq \frac{v\Gamma_a}{qV} (I_0 - I_{th})$

Decaiment : α_0



Equivalente elèctric

$$\omega_r^2 \triangleq \frac{1}{LC}$$

$$\frac{\omega_r^2}{2\alpha_0} \triangleq \frac{1}{RC}$$

- Naturalesa aleatòria de la llum

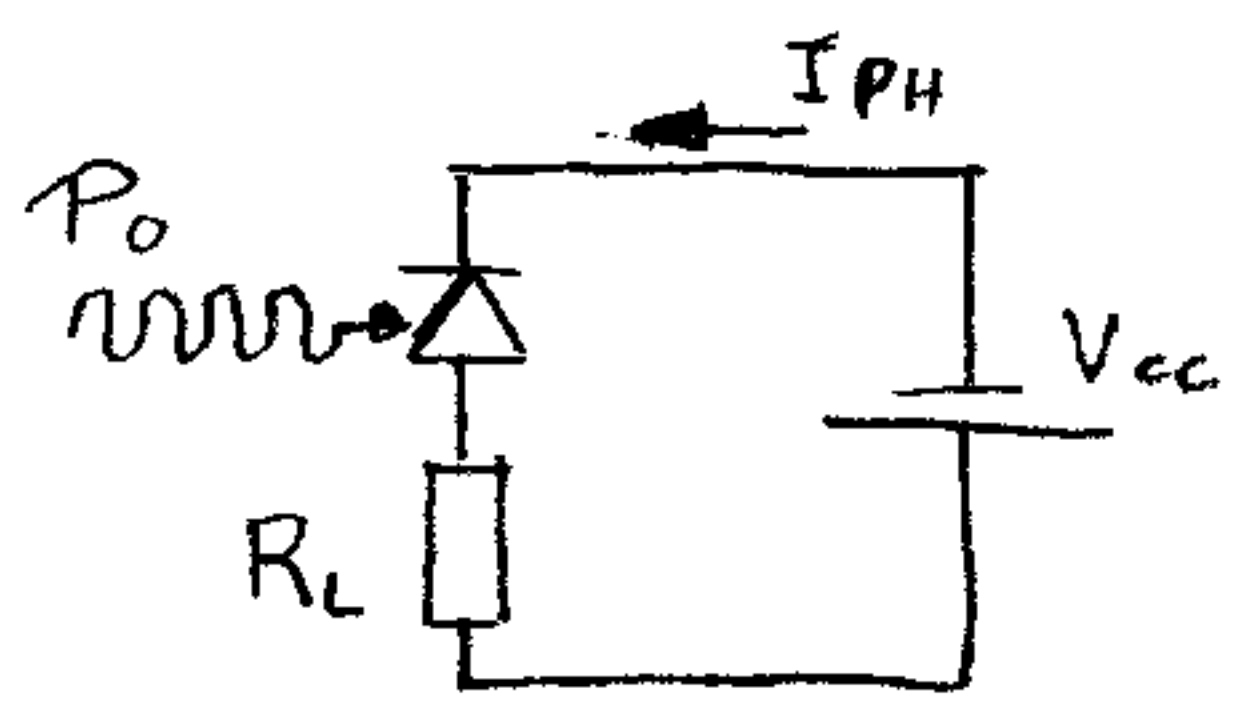
LASER $\left\{ \begin{array}{l} \langle m \rangle \\ \sigma_m^2 = \langle m \rangle \end{array} \right.$

$$SNR \triangleq \langle m \rangle$$

LED $\left\{ \begin{array}{l} \langle m \rangle \\ \sigma_m^2 = \langle m \rangle^2 + \langle m \rangle \end{array} \right.$

$$SNR = \frac{\langle m \rangle^2}{\langle m \rangle^2 + \langle m \rangle} \approx 1$$

1-4 RECEPTORS OPTICS

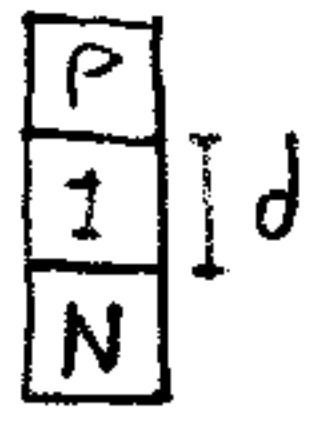


Eficiencia quàntica

$$\eta \triangleq \frac{I_{PH}/q}{P_{IN}/h\nu}$$

Responsivitat

$$R \triangleq \frac{I_{PH}}{P_{IN}} = \eta \frac{q}{h\nu}$$



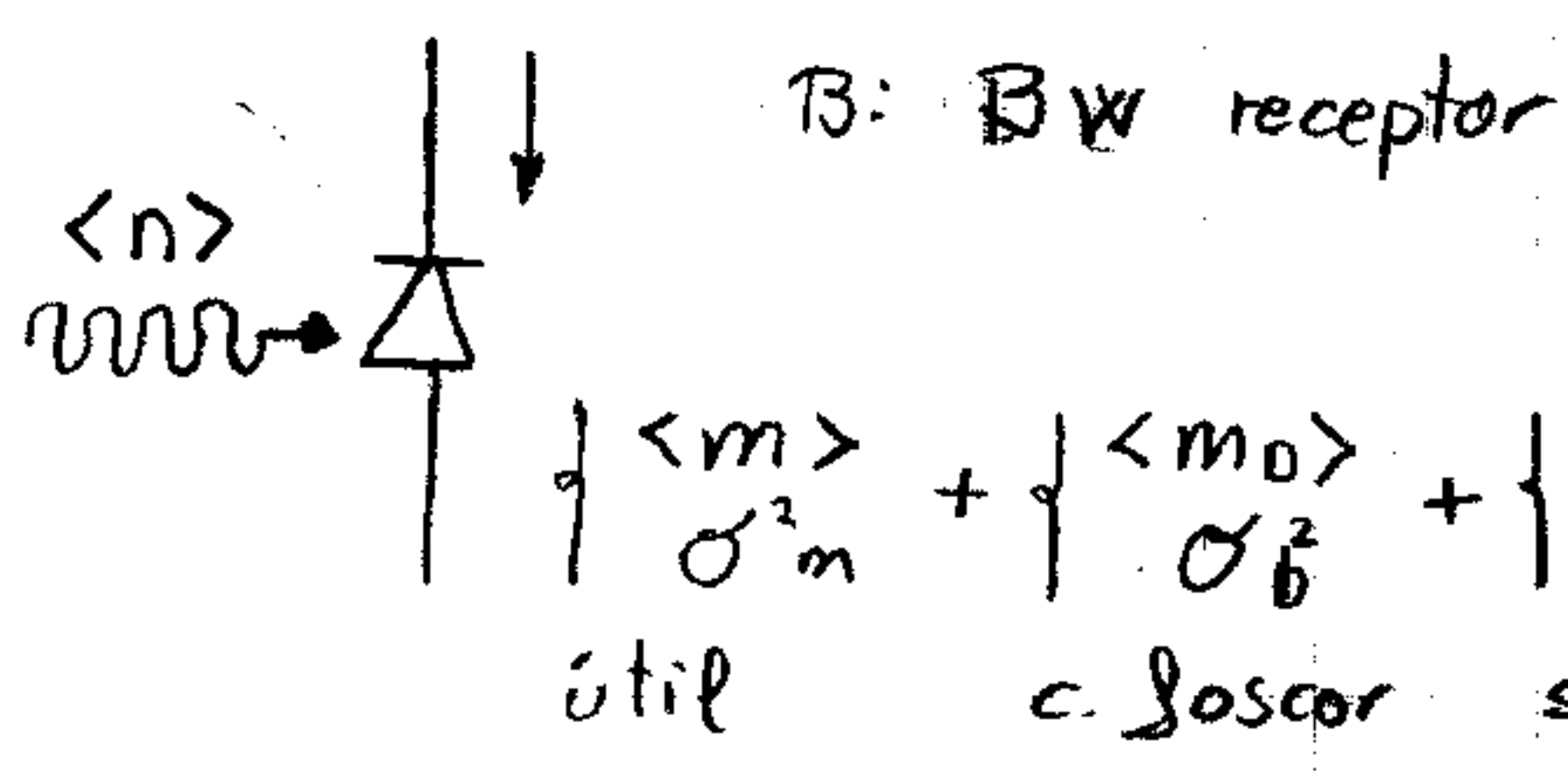
$$\eta \triangleq \frac{P_{absorbida}}{P_{incident}} \cong (1-R)(1-e^{-\alpha_p d}) \quad \alpha_p: \text{coef. absorció}$$

- FOTODIODE PIN

$$I_{PD} = I_{PH} + I_D$$

(fotocorrent) + (corrent de foscor)

Variables normalitzades



$$\langle I_{PH} \rangle \rightarrow \langle m \rangle = \frac{\langle I_{PH} \rangle}{2Bq}$$

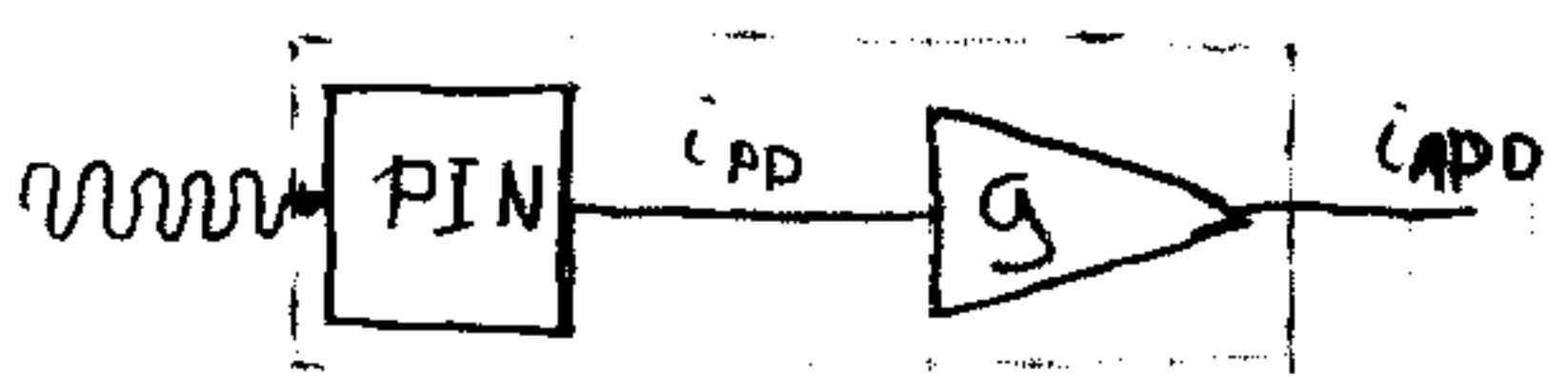
$$\sigma_{PH}^2 \rightarrow \sigma_m^2 = \frac{\sigma_{PH}^2}{(2Bq)^2}$$

$$\left. \begin{aligned} I_{PH} &\triangleq \langle I_{PH} \rangle = R \cdot P_{IN} \\ \sigma_{PH}^2 &= 2qB \cdot I_{PH} \end{aligned} \right\} \begin{aligned} \langle m \rangle &= \eta \langle n \rangle \\ \sigma_m^2 &= \langle m \rangle \end{aligned}$$

$$SNR^{PIN} = \frac{I_{PH}^2}{2Bq(I_{PH} + I_D) + \sigma_{th}^2}$$

$$SNR_{max}^{PIN} = \frac{\langle I_{PH} \rangle}{2Bq}$$

- FOTODIODE APD



$$M = \langle g \rangle$$

NF: Figura de soroll

$$\left. \begin{aligned} \langle I_{APD} \rangle &= M \langle I_{PD} \rangle \\ \sigma_{APD}^2 &= M^2 NF \cdot \sigma_{PD}^2 \end{aligned} \right\} \begin{aligned} \langle m \rangle_{APD} &= M \langle m \rangle \\ \sigma_{m,APD}^2 &= M^2 \cdot NF \cdot \langle m \rangle \end{aligned}$$

$$SNR^{APD} = \frac{M^2 I_{PH}^2}{2Bq M^2 NF (I_{PH} + I_D) + \sigma_{th}^2}$$

$$SNR_{max}^{APD} = \frac{\langle I_{PH} \rangle}{2Bq NF}$$

- Comparació PIN-APD ($I_0 = 0$)

$$\text{SNR}_{\text{PIN}} = \frac{\langle m \rangle^2}{\langle m \rangle + \sigma_p^2}$$

$$\text{SNR}_{\text{APD}} = \frac{\langle m \rangle^2}{\text{NF} \langle m \rangle + \sigma_p^2 / M^2}$$

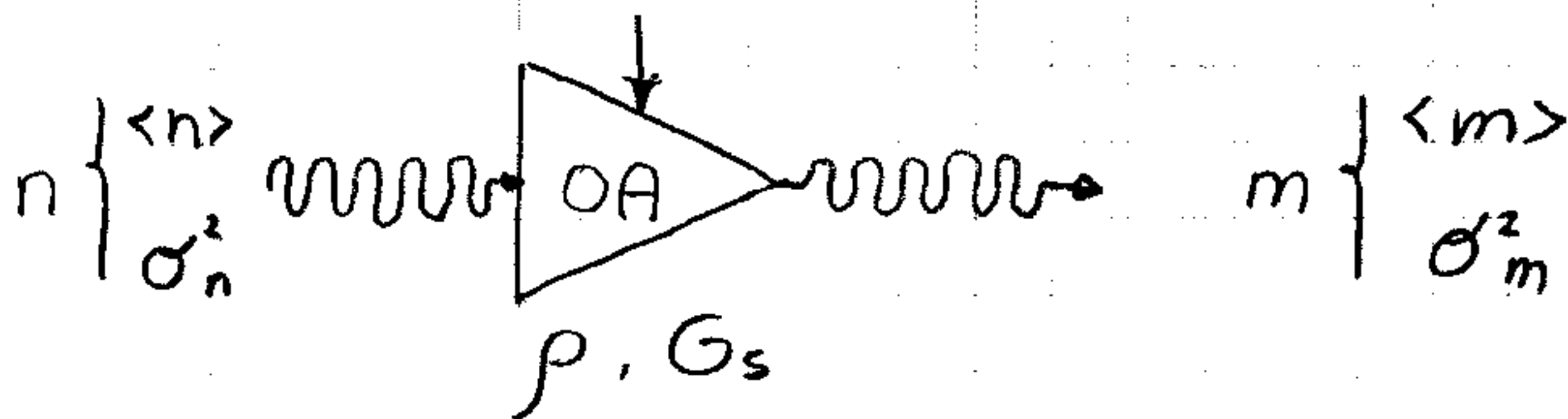
$$\text{APD mejor PIN} \Leftrightarrow \sigma_p^2 > (F-1) \langle m \rangle$$

$$\Rightarrow P_{\text{IN}} < \frac{h \nu}{\text{NF} \cdot \eta} 2B \sigma_p^2$$

T-5 AMPLIFICADORS ÒPTICS

SOA (Semiconductor Optical Amplifier)

EDFA (Erbium Doped Fiber Amplifier)



ρ : Emisió espontànea

G_s : Guany en passada única

$$\langle m \rangle = G_s \langle n \rangle + (G_s - 1) \rho$$

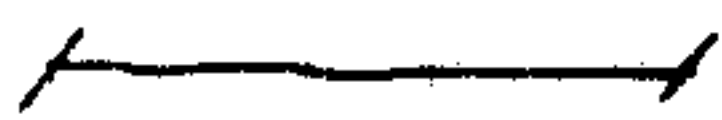
$$\sigma_m^2 \cong 2\rho G_s^2 \langle n \rangle$$

$$\sigma_m^2 = 2\rho G_s (G_s - 1) \langle n \rangle + \rho (G_s - 1)^2 + G_s^2 (\sigma_n^2 - \langle n \rangle) + G_s \langle n \rangle + \rho (G_s - 1)$$

$$\text{SNR}_{in} = \langle n \rangle$$

$$\text{SNR}_{out} = \frac{\langle n \rangle}{2\rho}$$

$$\text{NF} \cong 2\rho$$



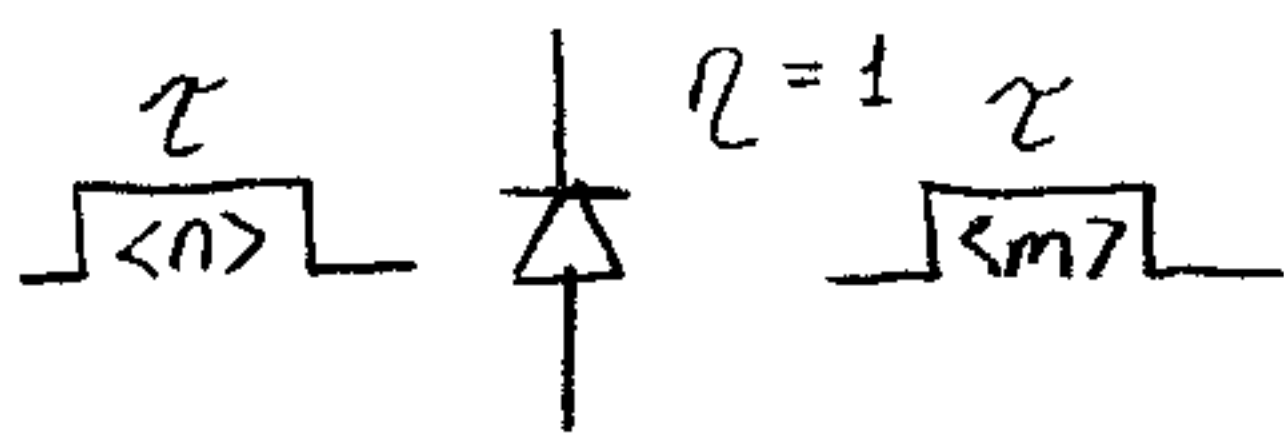
Amplificador Òptic: Funciona igual que un LASER però amb P_{in} i P_{out}

$$R_1 = R_2 = R \cong 10^{-5} \Rightarrow \text{Opera per sota de } I_{th}$$

$$G(\lambda) = \frac{G_s (1 - R)^2}{(1 - R G_s)^2 + 4 R G_s \sin^2(2\pi L / \lambda)}$$

1-6 SISTEMES DE TX PER F.O.

- Sistema totalment ideal



$$P(\epsilon) = \frac{1}{2} e^{-\langle n \rangle}$$

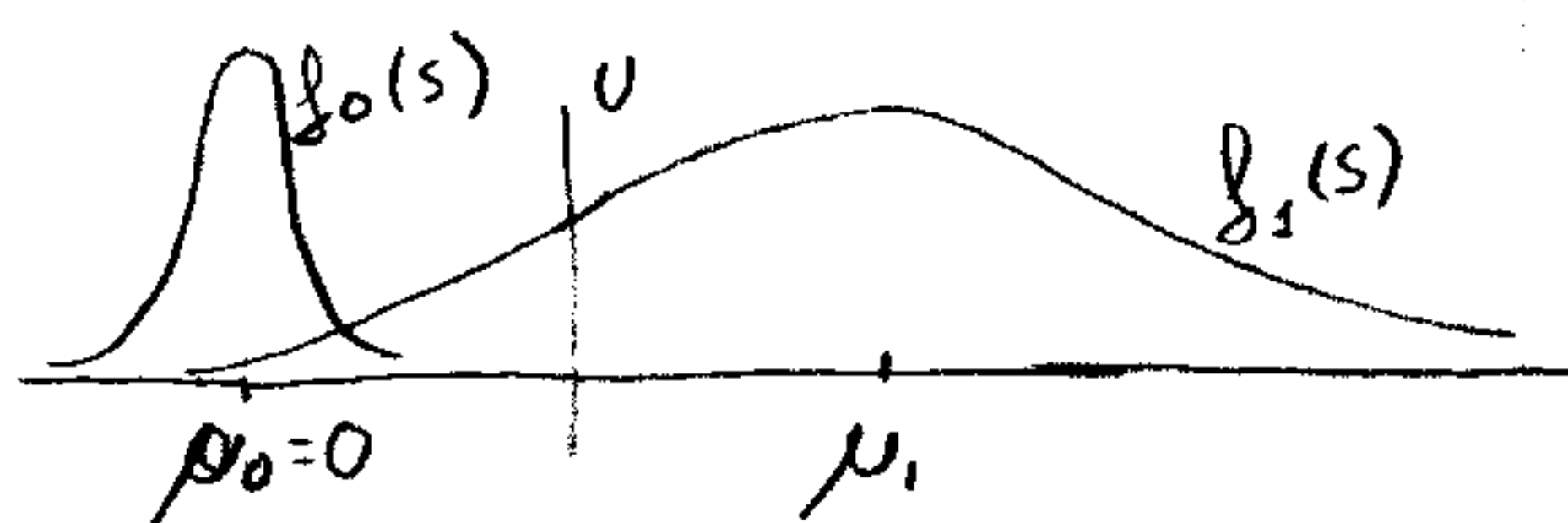
$$\text{BER} \triangleq \log P(\epsilon) = -0.3 - 0.87 \langle n \rangle$$

$$\langle n_a \rangle = \frac{\langle n \rangle_{b+0} + \langle n \rangle_{b+1}}{2} \Rightarrow \langle n_a \rangle = \frac{\langle n \rangle}{2}$$

$$\frac{1}{2} e^{-\eta \langle n \rangle}$$

Fotodiodo PIN con $\eta \neq 1 \Rightarrow \text{BER} = -0.3 - 0.87 \eta \langle n_a \rangle$

- Cas general



$$\sigma_0, \sigma_1 \ll |\mu_0 - \mu_1|$$

$$N_{\text{opt}} \approx \frac{\mu_0 \sigma_1 + \mu_1 \sigma_0}{\sigma_1 + \sigma_0}$$

$$P_{\min}(\epsilon) = \frac{1}{2} \left[1 + \frac{1}{2} \operatorname{erf} \left(\frac{u_{\text{opt}} - \mu_1}{\sqrt{2} \sigma_1} \right) - \frac{1}{2} \operatorname{erf} \left(\frac{u_{\text{opt}} - \mu_0}{\sqrt{2} \sigma_0} \right) \right]$$

- Paràmetres Q

si $u = u_{\text{opt}} \Rightarrow Q = \frac{\mu_1 - \mu_0}{\sigma_1 + \sigma_0}$

• 1a Situació: Domina soroll shot $\sigma_1^2 \gg \sigma_0^2$

$$\text{SNR} \approx Q^2$$

• 2a Situació: Domina soroll tèrmic $\sigma_1^2 \approx \sigma_0^2$

$$\text{SNR} \approx 4Q^2$$

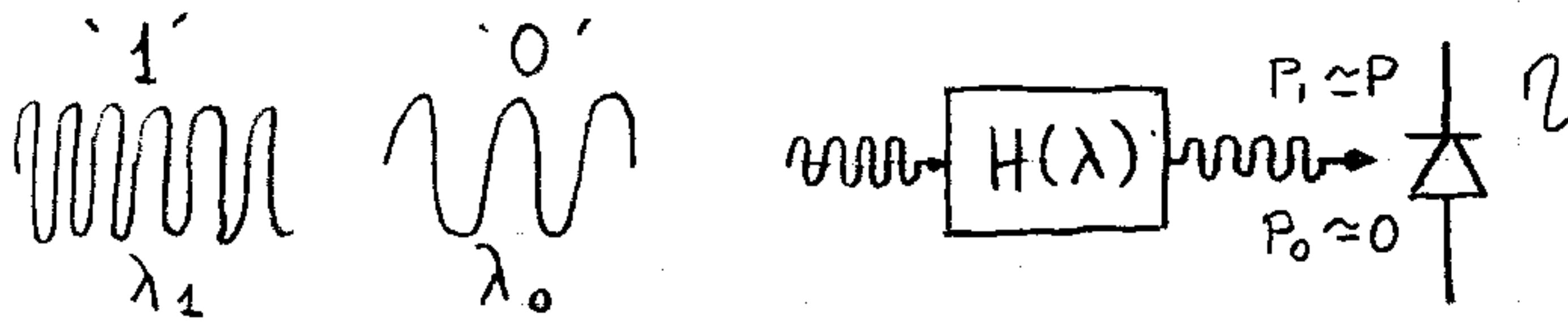
• Cas general

$$\frac{\sqrt{\text{SNR}}}{2} \leq Q \leq \sqrt{\text{SNR}}$$

$$P_{\min}(\epsilon) = \frac{1}{2} \left[1 - \operatorname{erf} \frac{Q}{\sqrt{2}} \right] = \frac{1}{2} \operatorname{erfc} \frac{Q}{\sqrt{2}}$$

Per $P_{\min}(\epsilon) < 10^{-9} \Rightarrow Q \geq 6$

- FSK Optic



$$\begin{array}{l}
 \langle n_1 \rangle \uparrow \eta \\
 \langle n_0 \rangle \uparrow + \sigma_p^2
 \end{array}
 \left. \begin{array}{l}
 '1' \\
 '0'
 \end{array} \right\}
 \begin{array}{l}
 \langle m_1 \rangle = \eta \langle n_1 \rangle \\
 \sigma_1^2 = \eta \langle n_1 \rangle + \sigma_p^2 \\
 \langle m_0 \rangle = \eta \langle n_0 \rangle \\
 \sigma_0^2 = \eta \langle n_0 \rangle + \sigma_p^2
 \end{array}$$

$$Q \approx \frac{\eta \langle n_1 \rangle}{\sqrt{\eta \langle n_1 \rangle + \sigma_p^2} + \sqrt{\sigma_p^2}}$$

• Cas 1 : Dominant shot noise $\Rightarrow \eta \langle n_1 \rangle \gg \sigma_p^2$

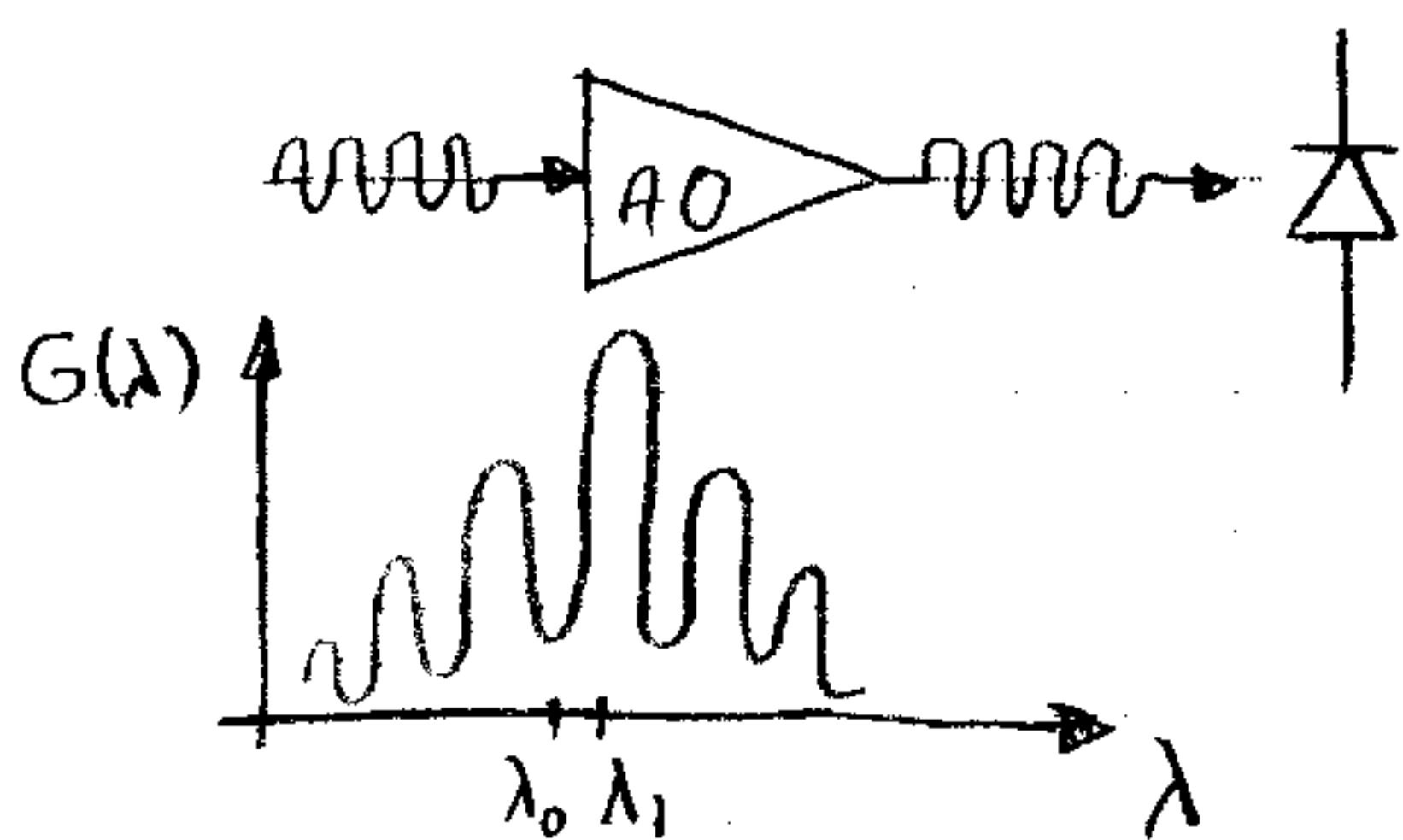
$$Q \approx \sqrt{\eta \langle n_1 \rangle} \stackrel{!!}{\geq} 6 \Rightarrow \langle n_1 \rangle = \frac{36}{\eta}$$

• Cas 2 : Shot noise order of thermal noise $\Rightarrow \sigma_p^2 \approx \eta \langle n_1 \rangle$

$$Q \approx \frac{\sqrt{\eta \langle n_1 \rangle}}{1 + \sqrt{2}} \stackrel{!!}{\geq} 6 \Rightarrow \langle n_1 \rangle = \frac{210}{\eta}$$

• Cas réel (intermittent) $\Rightarrow \frac{36}{\eta} < \langle n_1 \rangle < \frac{210}{\eta}$

- FSK Optic + PAO



$$\langle n_1 \rangle \geq 72 \rho$$

- Model estadístic d'un AO (Ampliació)

$$\begin{cases} \langle m \rangle = G_s \langle n \rangle + \rho (G_s - 1) \\ \sigma_m^2 = 2\rho G_s (G_s - 1) \langle n \rangle + \rho^2 (G_s - 1)^2 + G_s^2 (\sigma_n^2 - \langle n \rangle) + G_s \langle n \rangle + \rho (G_s - 1) \end{cases}$$

En general $\sigma_n^2 > n \Rightarrow \sigma_n^2 = \alpha \langle n \rangle$

$$SNR_{IN} = \frac{\langle n \rangle}{\alpha} \quad SNR_{OUT} = \frac{\langle n \rangle}{\alpha - 1 + 2\rho} \quad NF = \frac{\alpha - 1 + 2\rho}{\alpha}$$

o Cas particular: Fibra òptica $\rho = 0$; $G_s = A < 1$

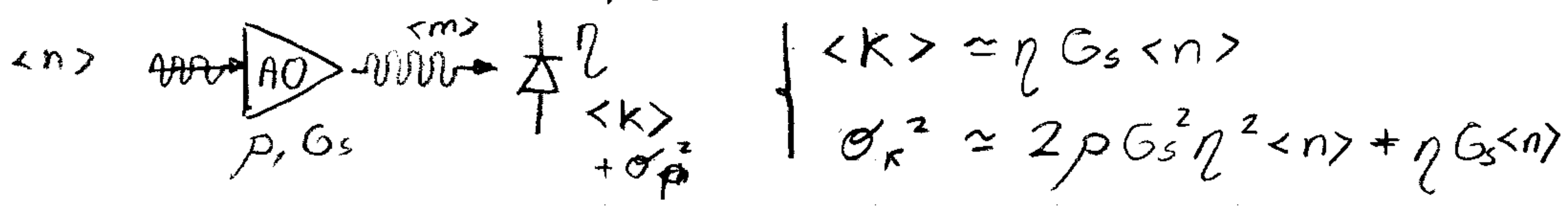
$$\begin{cases} \langle m \rangle = A \langle n \rangle \\ \sigma_m^2 = A^2 (\sigma_n^2 - \langle n \rangle) + A \langle n \rangle = \downarrow \text{alum coherent } \sigma_n^2 = \langle n \rangle \quad A \langle n \rangle = \langle m \rangle \end{cases}$$

$$SNR_{IN} = \langle n \rangle \quad SNR_{OUT} = A \langle n \rangle \quad NF = 1/A$$

o Cas particular: Fotodiode $\rho = 0$; $G_s = \eta$

Idem Fibra amb $A = \eta$

o Cas particular: Preamplificador + Fotodiode

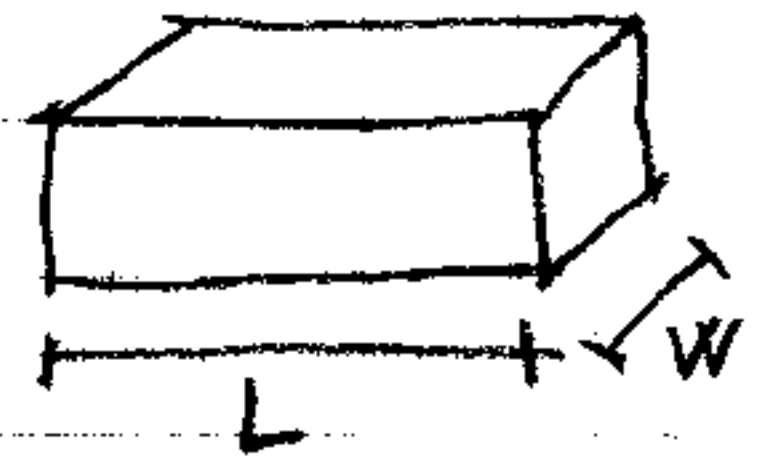


$$SNR_{IN} = \langle n \rangle$$

$$\text{Si } G_s^2 \gg \frac{\sigma_p^2}{2\rho\eta^2\langle n \rangle} \Rightarrow SNR_{OUT} = \frac{\langle n \rangle}{2\rho} \quad NF = 2\rho$$

⇒ Tenim la mateixa SNR que només amb el AO

- Reflectivitats $R_1, R_2, R_1 = R_2 = 0$
- Nivel de transparència N_0
- Paràmetre de emissió espontànea β
- Factor de confinament Γ
- Perdues scattering α_s
- Corriente umbral I_{th}



Ecs. ritme Laser:

Portadors $\frac{dN}{dt} = \frac{I}{q \cdot V} - \frac{N}{\tau_r} - v \cdot g \cdot S$

~~$I = I \cdot w \cdot L \cdot w$~~

Fotons $\frac{dS}{dt} = \frac{v \cdot g \cdot S - v \cdot \alpha_t \cdot S + \beta \cdot \frac{N}{\tau_r}}{v \cdot (g - \alpha_t) \cdot S}$

- N densitat portadors zona activa
- τ_r temps de vida del portador
- g guany per emissió estimulada neta
- α_t perdues totals en la cavitat
- τ_p temps permanència fotó a la cavitat
- S densitat de fotons
- a coeficient de guany
- γ factor de curvatura
- g_p guany màxim
- g_n guany net de la llum al medi
- g_m guany del material

-
- I_d corriente oscuridad media
 - I_{PH} fotocorriente media
 - I_{TH} corriente de ruido termico media

$\langle i_{th} \rangle = 0$

$\sigma_{th}^2 = \langle i_{TH}^2 \rangle = 4 \frac{kT B F_n}{R_L}$

$N_{th} = N_0 + \frac{\alpha_t}{\Gamma a}$

$\beta B_c = \frac{v \tau_r}{2}$

$\sigma \cdot B_c = \frac{0.1874}{\sqrt{2}}$